

Performance Comparison of Neural Network Based Multi Output SMPS with Improved Power Quality and Voltage Regulation.

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Abstract: In this paper a neural network based Switched Mode Power Supply (SMPS) of 175W rating is designed with $\pm 5V$ and $\pm 12V$ employing various converter topologies and simulated in MATLAB to demonstrate improved power quality in terms of low total harmonic distortion of supply current, high power factor, distortion factor and displacement factor. The performance of SMPS is analyzed based on input power quality, output voltage regulation and transient response under varying source and load conditions. Comparison of performances with neural network and conventional controllers highlight the neural network control. The converter with superior performance is adopted for developing hardware.

Keywords: Switched mode power supply, power quality, total harmonic distortion and power factor

1. INTRODUCTION

Switched Mode Power Supplies (SMPS), Uninterruptible Power Supplies (UPS), battery chargers, electronic ballasts, Adjustable Speed Drives (ASDs) etc., extensively utilize the solid state AC-DC converters with High Frequency Transformer (HFT) isolation (Moore and Portugues, 2003). In conventional topology, the AC-DC converters are designed with two stages. The first stage of the topology incorporates Diode Bridge Rectifier (DBR) which rectifies input AC voltage into an uncontrolled DC voltage. The second stage of the circuit constitutes, a high frequency isolation transformer and a DC-DC converter which is cascaded with first stage. The two stage AC-DC converters introduce Power Quality (PQ) problems and increase the size of the DC capacitor in the first stage (Carlos et al., 2010). The major power quality issues are harmonic current injection into the AC mains, distortion of source voltage and decrease in power factor (PF) (Jingquan et al., 2006). Due to increased application of AC-DC converters, the researchers focused on the development of single stage converters which mitigate the PQ problems, improve the efficiency and reduce the overall cost of the system by employing less number of components (Shika Singh et al., 2015; Singh et al., 2003; Singh et al., 2011; Woo and Joo, 2011). The proposed single stage topology of AC-DC converter with HFT isolation overcomes all the drawbacks of two-stage converters and improves the PQ. This paper deals with the performance analysis of Artificial Neural Network (ANN) based Multiple Output Switched Mode Power Supply (MOSMPS) involving various converter topologies with HFT isolation. Various converter topologies like forward, sepic, cuk and flyback are designed and implemented with multiple outputs of $\pm 12V$ and $\pm 5V$ for a load rating of 175W mainly used in the PC power supply application. The HFT has a single primary winding and multiple number of secondary windings to accomplish four different outputs. The closed loop control employs a NN based weighted error approach for power quality

improvement at the source side to meet the IEEE 519 and IEC 61000-3-2 standards and for output voltage regulation. The modeling and performance analysis of various converter topologies under varying source and load conditions are performed in MATLAB Simulink environment. The performance of various converter topologies are evaluated based on the PQ indices such as Total Harmonic Distortion (THD), Power factor, Displacement Power Factor (DPF) and Distortion Factor (DF) and output voltage regulation in terms of voltage ripple. The performance of the MOSMPS with neural network controller is compared with that of MOSMPS with conventional controller. The converter topology which performs better in all aspects of power quality indices and output voltage regulation is chosen and the prototype model is developed. The proposed NN based control strategy is implemented in hardware using FPGA processor. The results of the developed prototype model are compared with simulation results confirming the validity of the design.

2. SYSTEM CONFIGURATION

The system configuration of SMPS with multiple isolated outputs is shown in Fig. 1. A DBR is employed at the input side of MOSMPS which rectifies the sinusoidal voltage V_{in} of the ac mains.

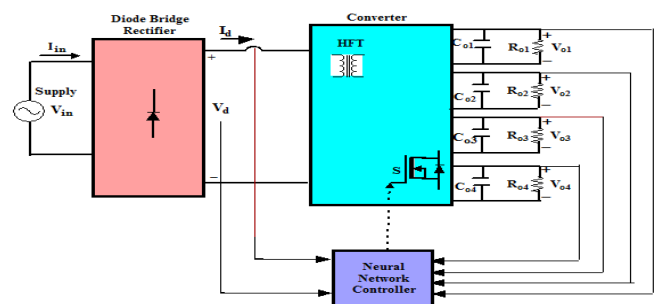


Fig. 1 System Configuration of MOSMPS

The unregulated output of the DBR is fed to a DC-DC converter in order to regulate the DC voltage. The regulated DC voltage is applied to a HFT, which helps in the isolation of various multiple DC outputs and voltage scaling. The four multiple output voltages V_{01} , V_{02} , V_{03} and V_{04} of MOSMPS are derived from the secondary windings of HFT. The performance of converter in terms of output voltage regulation and power quality improvement at the input side depends on the choice of the control strategy.

2.1 Forward Converter

Fig. 2 depicts the forward converter configuration of MOSMPS with NN based weighted error control approach. In this topology the primary side of the HFT is connected to, the components of DBR, L_i , C_i and diodes (D_{i1} and D_{i2}). The secondary windings of the HFT are connected to inductors L_{01} thru L_{04} , diodes D_{01} thru D_{08} , and capacitors C_{01} thru C_{04} . The value of capacitor C_i is chosen as large as possible in order to maintain the ripple content of voltage as small as possible (Chow et al., 1998).

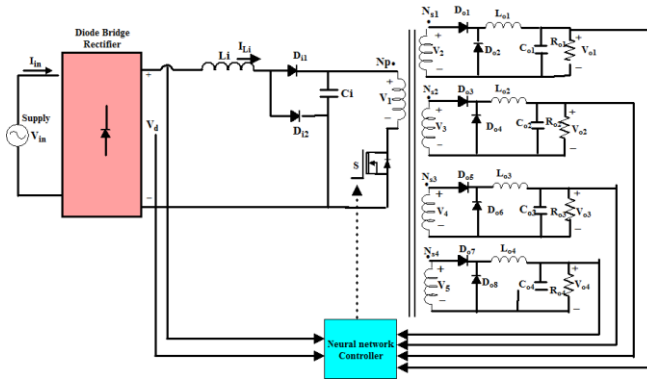


Fig. 2 Forward Converter based MOSMPS

The second order harmonic voltage at the output side is filtered out using the capacitors C_{01} to C_{04} . The diode D_{i2} becomes forward biased and D_{i1} becomes reverse biased when the switch S is turned ON. Under OFF condition of the switch, the energy is transferred to the loads through Diode D_{i1} . The converter employs Metal Oxide Semiconductor Field Effect Transistor (MOSFET) as switching device. This topology results in reduction in the, number of components, cost, losses and size of the inductors.

2.2 Sepic Converter

Fig. 3 depicts the SEPIC converter configuration of MOSMPS with NN based weighted error control. The input inductor L_i acts as energy storage element, which stores energy when the switch S is turned ON through the AC source mains (Buso et al., 2000). When the switch is turned OFF the load receives energy from the inductor and it also charges the capacitor C_1 . DC capacitors C_{01} thru C_{04} act as filter capacitors for filtering out the ripples present in DC output voltages. The SEPIC converter has improved PQ performance in the input side.

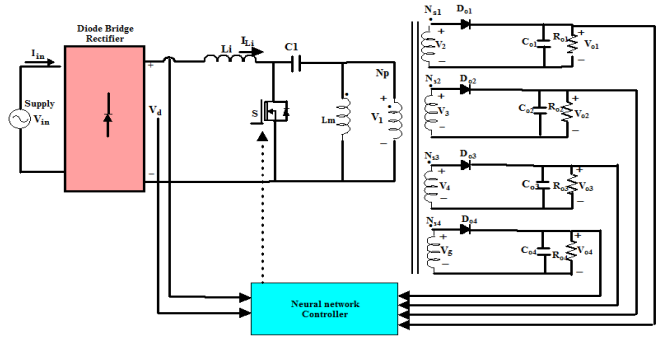


Fig. 3. Sepic Converter based MOSMPS

2.3 Cuk Converter

Fig. 4 depicts the cuk converter configuration of MOSMPS with NN based weighted error control. Capacitor C_{10} acts as energy transfer capacitor on the primary side and capacitors C_{11} thru C_{14} act as energy transfer capacitors on the secondary side of the HFT for multiple output voltages (Buso et al., 2000). The inductors with appropriate value also aid the energy transfer both in primary and secondary sides. The primary side capacitor C_{10} gets charged when the switch S is turned OFF which in turn makes the diodes (D_1 , D_2 , D_3 , and D_4) present on the secondary side to be forward biased. Under ON condition of the switch, the diodes on the secondary side become reverse biased due to the voltage across the capacitor. Thus the energy stored in the capacitor is discharged to the load via the switch S .

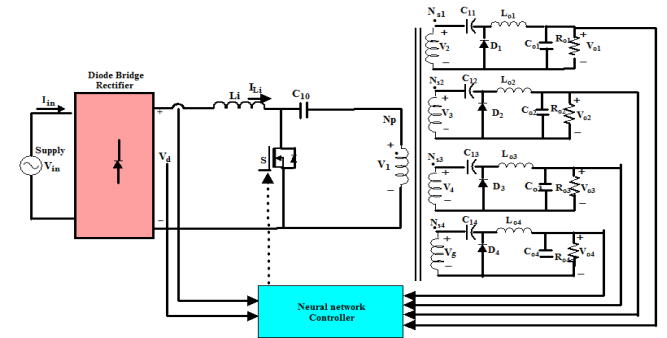


Fig. 4 Cuk Converter based MOSMPS

2.4 Flyback Converter

Fig. 5 depicts the fly back converter configuration of MOSMPS with NN based weighted error control. The inductor stores energy when the switch S is in ON condition and discharges the energy when it is in OFF condition. Under charging condition, the diodes at the secondary windings of HFT are under reverse biased condition and during discharging condition the diodes become forward biased, thus transferring the energy stored in the inductors to pass on to the load. Duty ratio plays an important role, as the energy drawn by the load should be equal to the energy stored in the inductor L_m (Zhao et al., 2002).

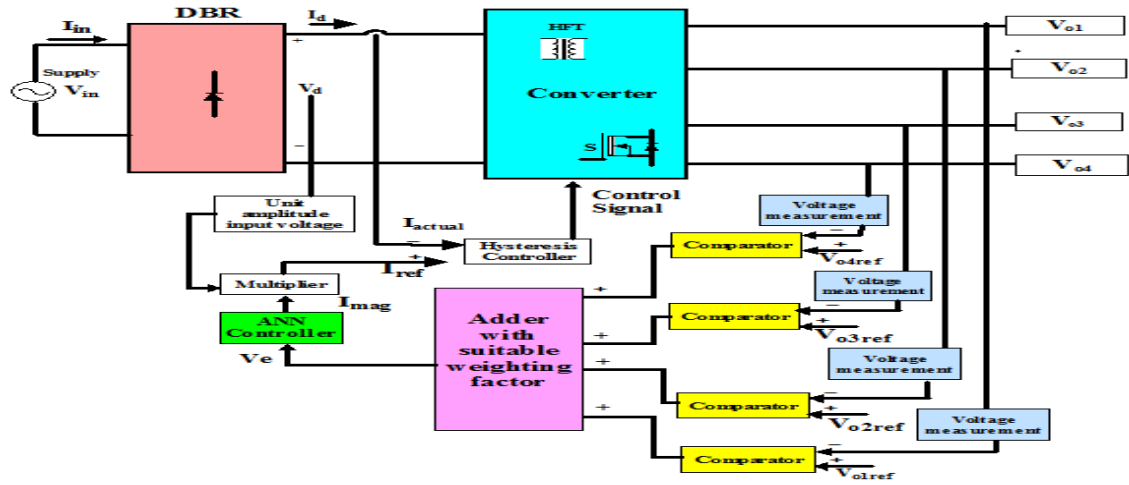


Fig. 6 Schematic Diagram of Neural Network based Weighted Error Approach.

of neurons in the hidden layer and MSE are not directly related in the training process. The highest value of R^2 and minimum value of MSE are achieved when the number of neurons is 20 in the hidden layer. The details of ANN parameters of various converter topologies for training in MATLAB are listed in Table 2. The four axes shown in Fig. 9 represent training, validation, testing and total response of the data for NN control strategy in forward converter. The dotted line in each axis represents the perfect results where outputs = targets. The solid line represents the best fit linear regression line between outputs and targets. The R value is an indication of the relationship between the outputs and targets. If $R=1$, it indicates that there is an exact linear relationship between outputs and targets. If R is zero, then there is no linear relationship between outputs and targets. The output tracks the target very well for training, testing and validation and the R-value is over 0.96 for the total response. Fig. 10 depicts the performance curve of NN control for forward converter and it is inferred that error decreases as the number of epochs increases and converges to a value of 0.00109 after 1000 epochs to reach the goal.

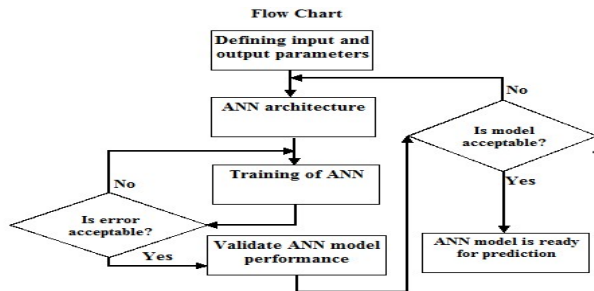


Fig. 7 Flow chart of ANN modelling

From the performance curve it can be inferred that, the results are reasonable because of the following considerations: i) The final mean square error is small, ii) The test set error and validation set error has similar characteristics and iii) No significant over fitting has occurred. The procedure followed

in neural network formulation for all other converters remains the same.

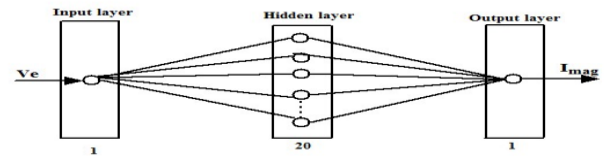


Fig. 8 Proposed BPNN architecture

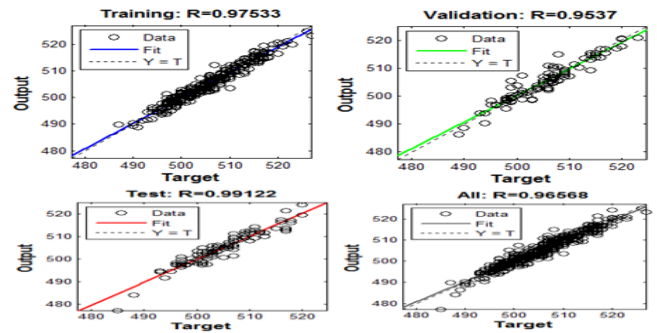


Fig. 9 (a) Training (b) Validation (c) Testing (d) Total response.

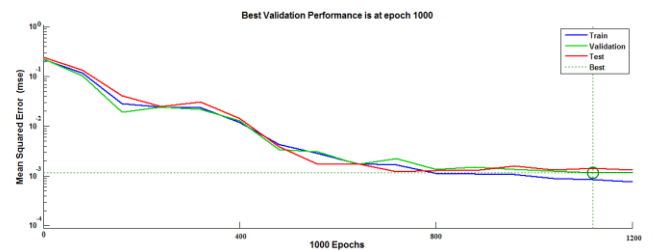


Fig. 10 The performance curve of NN Control for Forward Converter

Table 2. ANN parameters of various converter topologies

Parameter	Values			
	1*	2*	3*	4*
No of Training samples	1000	1000	1000	1000
No of Testing samples	200	200	200	200
Input layer neurons	1	1	1	1
Hidden layer neurons	20	24	26	30
Output layer neurons	1	1	1	1
Training function	LM Algorithm (trainlm)			
Performance function	Mean squared error (MSE)			
(input /hidden/output) Activation function	tansig/ tansig/ purelin			
Maximum no. of epochs	1000	920	210	920
Rate of Learning	0.05	0.05	0.05	0.05
Performance goal	$1e^{-3}$			
Normalized range	-1 to 1			
Accuracy of testing in %	99.1	99.23	99.21	99.23

1*- Forward converter, 2*-Sepic converter, 3*-Cuk converter & 4*-Flyback converter.

5. SIMULATION RESULTS AND DISCUSSIONS

To compare the performance of the multiple output SMPS of 175 W rating with different converter configurations, they are modeled as per the parameters specified in Table 3 and simulated using MATLAB /Simulink software. Power quality improvement at the input ac mains and output voltage regulations are achieved using the neural network controller. The simulation of the neural network based multi output SMPS with different converter configurations are carried out for validating their performance under i) steady state condition, ii) variable supply voltage and iii) varying loads. To validate the performance of the multiple output SMPS under varying source condition the source voltage is varied between 170V and 250V RMS and to highlight the performance under varying load condition the load at output terminal 2(V_{o2}) is increased from 50% to 100% at 0.5s of the simulation period.

Table 3. Parameters of MOSMPS

Sl.No.	Parameters	Values
1.	Supply voltage V_{in}	170-250 V RMS
2.	Switching frequency f_s	50 kHz
3.	Output voltage V_{o1}/I_{o1}	12 V/6 A
4.	Output voltage V_{o2}/I_{o2}	5 V/18 A
5.	Output voltage V_{o3}/I_{o3}	-5 V/0.3 A
6.	Output voltage V_{o4}/I_{o4}	-12 V/0.8 A
7.	Output power P_o	175 W

Tables 4 and 5 illustrate, the power quality indices of MOSMPS in terms of %THD of the supply current, DF, DPF, PF at the supply side and output voltage ripple for all

the four terminals with NN and conventional controller, at full load and 50% load condition respectively. Table 6 reports the comparison of performance of SMPS at full load with neural network and conventional controllers in terms of settling time, overshoot and undershoot of the output voltage at terminal 1.

5.1 Performance of forward converter based MOSMPS with NN controller

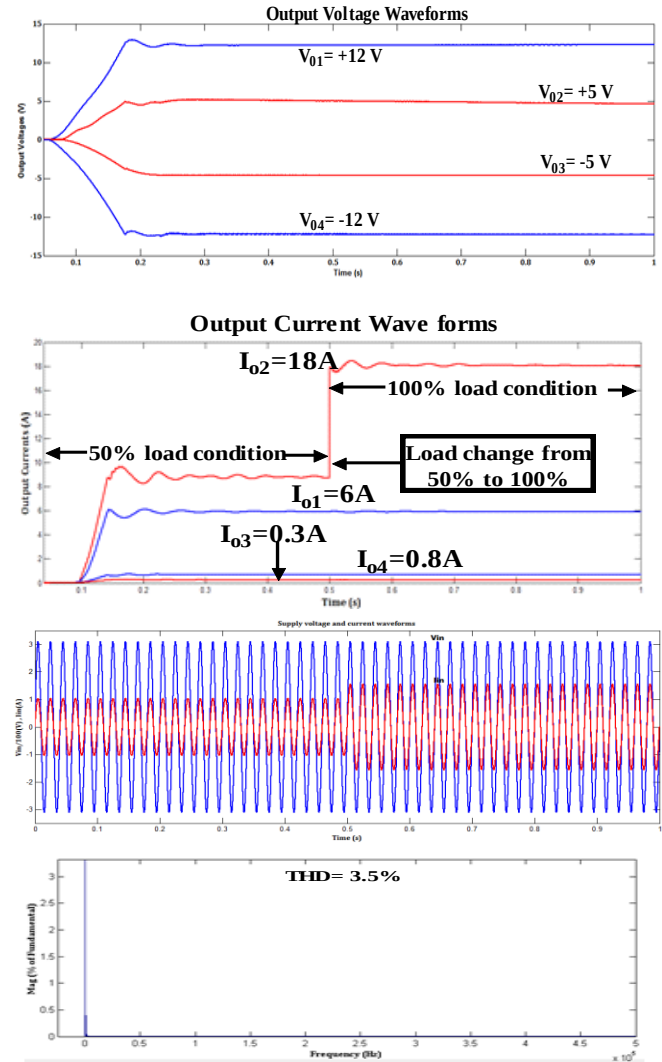


Fig. 11 Waveforms of forward converter based MOSMPS with $V_{in} = 220V$. Traces (a) Output voltages (V) (b) Output currents (A), (c) $V_{in}/100$ (V) and I_{in} (A), (d) %THD of I_{in}

Fig.11,12 and 13 depict the traces of regulated multiple output voltages, output currents, supply voltage and current with load variation and %THD of I_{in} for supply voltages 220V, 250V and 170V respectively. The output voltages are well regulated by the neural network controller even under load variation at terminal 2 from 50% to 100% at 0.5s. From the source voltage and current waveforms for $V_{in} = 220V$, it is evident that supply current drawn from the mains is sinusoidal and in phase with the supply voltage thereby

maintaining the power factor nearly unity. The values of DF, DPF and PF are 0.996, 1.00 and 0.996 respectively. The THD of the supply current is maintained at 3.5%. From the simulation results tabulated in Table 4 it is explicit that PF and THD achieved using conventional controller are 0.86 and 4.96% and this verifies the superior performance of the NN controller. Simulation results tabulated in Table 5 for light load condition also proves the efficacy of the proposed controller. From the traces for $V_{in} = 250V$, it is evident that, for increased supply voltage and load variation in terminal 2 at 0.5s, the neural network controller is able to, regulate the output voltages and maintain the supply current sinusoidal and in phase with the supply voltage. The values of DF, DPF and PF are 0.994, 1.00 and 0.994 respectively. The THD of the supply current is 4.33%. For decreased supply voltage of $V_{in} = 170V$ and load variation in terminal 2 at 0.5s, the neural network controller is able to, regulate the output voltages and maintain the supply current sinusoidal and in phase with the supply voltage. The values of DF, DPF and PF are 0.998, 1.00 and 0.998 respectively. The THD of the supply current is 2.15%. Forward converter based SMPS with NN controller takes 0.19s to attain steady state and the overshoot of V_{o1} is 1.85% during transient response. Table 6 justifies that transient response of the MOSMPS with NN controller is better than that of MOSMPS with conventional controller. For all cases of V_{in} the supply current THD is maintained below the limits of PQ standards.

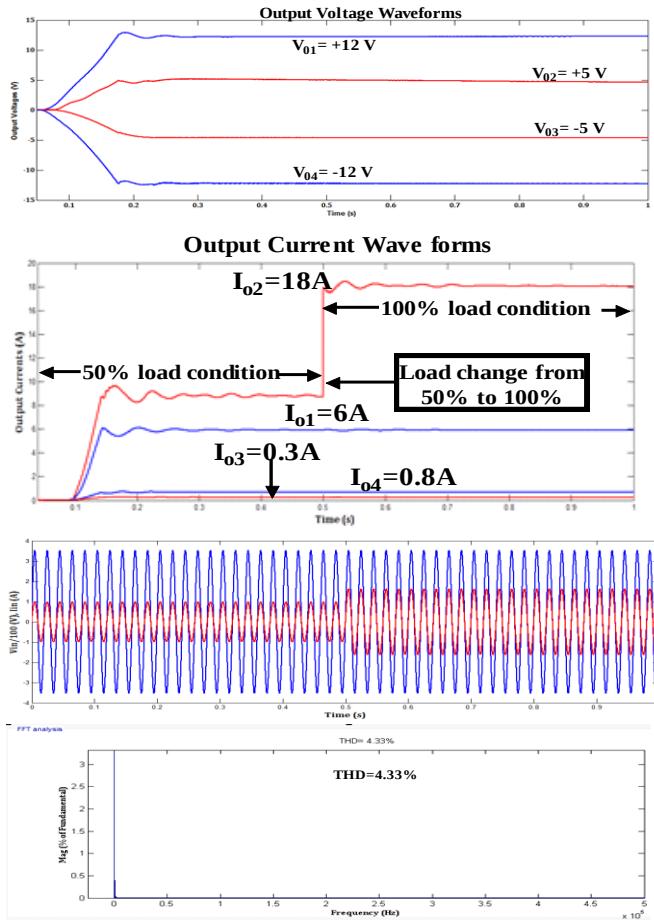


Fig. 12 Waveforms of forward converter based MOSMPS with $V_{in} = 250V$. Traces (a) Output voltages (V) (b)

Output currents (A), (c) $V_{in}/100$ (V) and I_{in} (A), (d) %THD of I_{in}

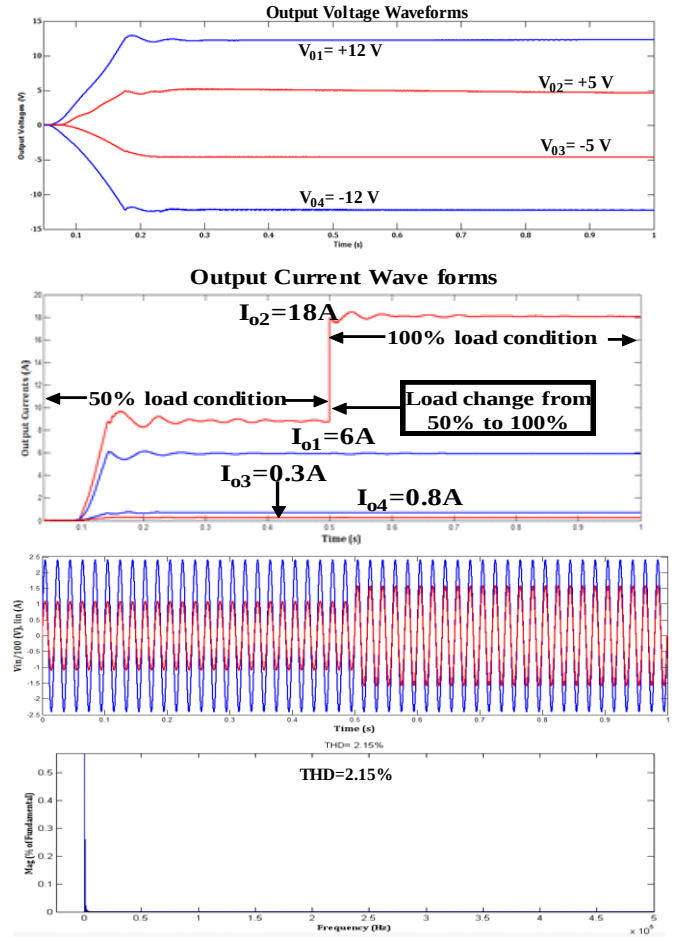


Fig. 13 Waveforms of forward converter based MOSMPS with $V_{in} = 170V$. Traces (a) Output voltages (V) (b) Output currents (A), (c) $V_{in}/100$ (V) and I_{in} (A), (d) %THD of I_{in}

5.2 Performance of sepic converter based MOSMPS with NN controller

Fig. 14 (a)-(c) depict the traces of regulated multiple output voltages for supply voltages 220V, 250V and 170V respectively. The output voltages are well regulated by the neural network controller. Supply currents drawn from the mains are sinusoidal and in phase with the supply voltage thereby maintaining the power factor nearly unity even under supply voltage variation from 170V to 250V. THD of the supply currents are 6.3%, 7.45% and 5.3 % and PF at the supply side are 0.976, 0.973 and 0.977 when the supply voltage is 220V, 250V and 170V respectively. Simulation results tabulated in Table 4 depicts that PF and THD achieved using conventional controller at $V_{in} = 220V$ are 0.81 and 7.2% and this verifies the superior performance of the NN controller. Simulation results tabulated in Table 5 for light load condition also proves the efficacy of the proposed controller. Sepic converter based SMPS takes 0.09s to attain

steady state. When compared to forward converter based SMPS, this SMPS takes lesser time to attain steady state. Sepic converter based SMPS has higher THD of source current for all the three cases of supply voltage when compared to forward converter based SMPS. For all the three cases of supply voltage THD of source currents do not satisfy the limit set by the standards IEC 61000-3-2. The overshoot of V_{01} is 2.2% during transient response. Table 6 proves that transient response of the MOSMPS with NN controller is better than that of MOSMPS with conventional controller.

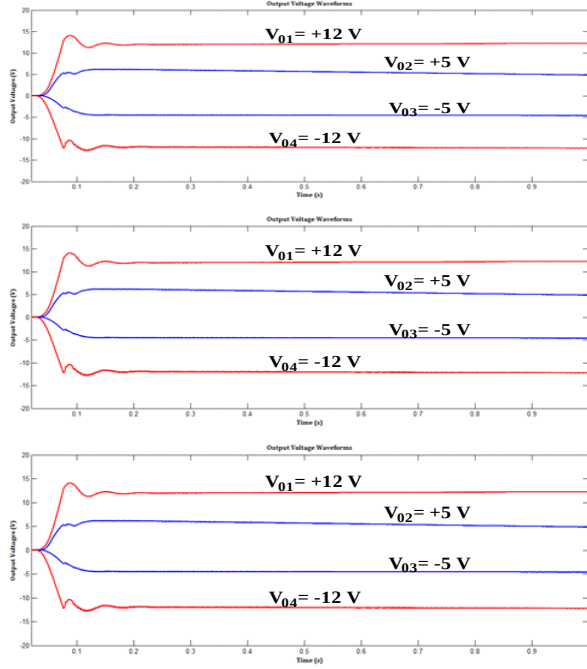


Fig. 14 Output voltages (V) of sepic converter based MOSMPS at (a) $V_{in} = 220V$ (b) $V_{in} = 250V$ (c) $V_{in} = 170V$

5.3 Performance of cuk converter based MOSMPS with NN controller

Fig. 15 (a)-(c) depict the traces of regulated multiple output voltages for supply voltages 220V, 250V and 170V respectively. The output voltages are well regulated by the neural network controller. THD of the supply currents are 4.6%, 4.9% and 3.9 % and PF at the supply side are 0.976, 0.975 and 0.978 when the supply voltages are 220V, 250V and 170V respectively. Supply currents drawn from the mains are sinusoidal and in phase with the supply voltage thereby maintaining the power factor nearly unity when the supply voltage is varied from 170V to 250V.

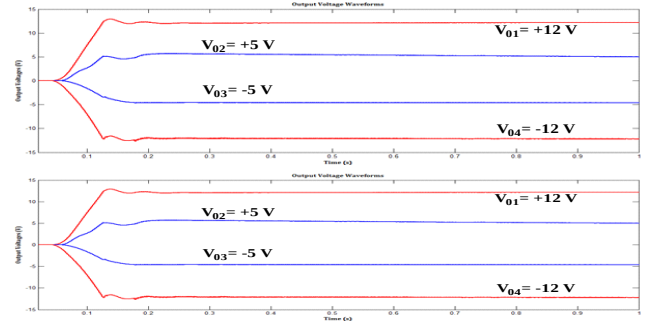
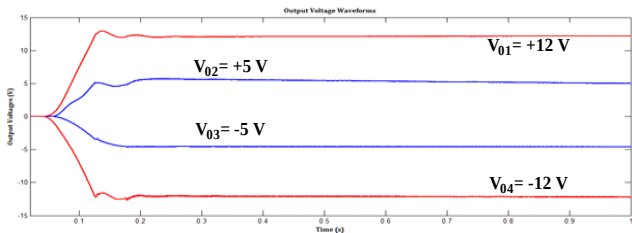


Fig. 15 Output voltages (V) of cuk converter based MOSMPS at (a) $V_{in} = 220V$ (b) $V_{in} = 250V$ (c) $V_{in} = 170V$

From the simulation results mentioned in Table 4 it is obvious that PF and THD achieved using conventional controller are 0.81 and 6.4% at $V_{in}=220V$ and this verifies the superior performance of the NN controller. Simulation results tabulated in Table 5 for light load condition also proves the efficacy of the proposed controller. Cuk converter based SMPS takes 0.23s to attain steady state. When compared to forward and sepic converter based SMPS, this SMPS takes more time to attain steady state. Cuk converter based SMPS has lower THD of source current for all the three cases of supply voltage when compared to sepic converter based SMPS. For all the three cases of supply voltage THD of source currents satisfy the limit set by the standards IEC61000-3-2. The overshoot of V_{01} is 2.2% during transient response. Performance comparisons listed in Table 6 demonstrate that transient response of the MOSMPS with NN controller is better than that of MOSMPS with conventional controller.

5.4 Performance of flyback converter based MOSMPS with NN controller

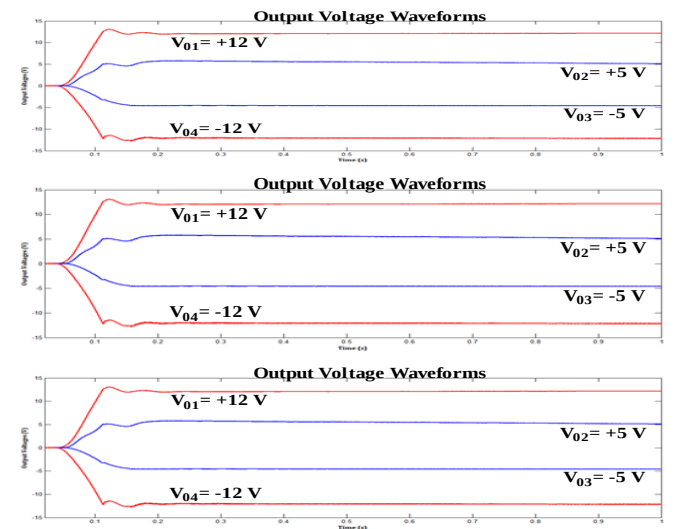


Fig. 16 Output voltages (V) of flyback converter based MOSMPS at (a) $V_{in} = 220V$ (b) $V_{in} = 250V$ (c) $V_{in} = 170V$.

Table 4. Parameter values under different supply voltages and 100% load condition at load terminals

Converter topology	Supply Voltage (V)	DF	DPF	PF		% THD of I_{in}		Output voltage ripple			
				1*	2*	1*	2*	V_{01} (%)	V_{02} (%)	V_{03} (%)	V_{04} (%)
Forward	170	0.998	1.00	0.998	0.84	2.15	3.87	1.6	1.9	1.3	1.0
	220	0.996	1.00	0.996	0.86	3.5	4.96				
	250	0.994	1.00	0.994	0.82	4.33	5.66				
Sepic	170	0.987	0.99	0.977	0.8	5.3	6.5	1.9	2.1	1.8	1.2
	220	0.986	0.99	0.976	0.81	6.3	7.2				
	250	0.983	0.99	0.973	0.84	7.45	8.9				
Cuk	170	0.988	0.99	0.978	0.77	3.9	5.5	1.8	2.3	1.6	1.6
	220	0.986	0.99	0.976	0.81	4.6	6.4				
	250	0.985	0.99	0.975	0.82	4.9	8.97				
Flyback	170	0.987	0.97	0.957	0.7	4.96	6.30	2.2	2.0	1.6	1.3
	220	0.986	0.97	0.956	0.79	5.2	7.8				
	250	0.983	0.97	0.953	0.84	6.3	10.56				

Table 5. Parameter values under different supply voltages and 50% load condition at load terminal 2.

Converter topology	Supply Voltage (V)	DF	DPF	PF		% THD of I_{in}		Output voltage ripple			
				1*	2*	1*	2*	V_{01} (%)	V_{02} (%)	V_{03} (%)	V_{04} (%)
Forward	170	0.998	0.99	0.988	0.75	4.36	5.86	1.3	1.5	1.2	1.0
	220	0.996	0.99	0.986	0.78	5.00	7.07				
	250	0.994	0.99	0.984	0.80	6.23	9.54				
Sepic	170	0.985	0.99	0.975	0.81	5.1	6.9	2.3	2.1	1.6	1
	220	0.984	0.99	0.974	0.79	6.85	7.3				
	250	0.983	0.99	0.973	0.76	7.63	9.2				
Cuk	170	0.987	0.99	0.977	0.76	4.1	6.2	0.9	1.3	1.2	1.2
	220	0.983	0.99	0.973	0.83	5.3	7.8				
	250	0.981	0.99	0.971	0.80	6.8	9.3				
Flyback	170	0.988	0.97	0.958	0.72	5.2	7.5	2.0	1.8	1.4	1.2
	220	0.986	0.97	0.956	0.73	6.4	7.9				
	250	0.984	0.97	0.954	0.82	7.1	9.32				

Table 6. Comparison of performance of SMPS at rated voltage with neural network and conventional controllers.

Converter topology	Power Density	Cost	Settling Time (s)		Transient Response of V_{o1} with NN Control		Transient Response of V_{o1} with Conventional Control	
			1*	2*	Overshoot (%)	Undershoot (%)	Overshoot (%)	Undershoot (%)
Forward	low	medium	0.19	0.23	1.85	2.00	2.25	2.32
Sepic	medium	medium	0.09	0.14	2.2	2.34	2.9	2.83
Cuk	medium	Medium	0.23	0.25	2.2	2.3	2.9	2.67
Flyback	low	Low	0.24	0.26	2.3	2.52	2.85	2.86

1*-NN Controller, 2*-Conventional Controller

Fig. 16 (a)-(c) depict the traces of regulated multiple output voltages for supply voltages 220V, 250V and 170V respectively. The output voltages are well regulated by the neural network controller. Supply currents drawn from the mains are sinusoidal and in phase with the supply voltage thereby maintaining the power factor nearly unity when the supply voltage is varied from 170V to 250V. THD of the supply currents are 5.2%, 6.3% and 4.96 % and PF at the

supply side are 0.956, 0.953 and 0.9576 when the supply voltages are 220V, 250V and 170V respectively. From the simulation results tabulated in Table 4 it is explicit that PF and THD achieved using conventional controller are 0.79 and 7.8% at $V_{in}=220V$ and this verifies the superior performance of the NN controller. Simulation results tabulated in Table 5 for light load condition also proves the efficacy of the proposed controller. Flyback converter based SMPS takes

0.24s to attain steady state. Flyback converter based SMPS takes more time to attain steady state when compared to other converter based SMPS. Flyback converter based SMPS has lower THD of source current for all the three cases of supply voltage when compared to sepic converter based SMPS but THD values of supply current do not satisfy the limit set by the standard IEC 61000-3-2. The overshoot of V_{o1} is 2.3% during transient response. Performance comparisons listed in Table 6 demonstrate that transient response of the MOSMPS with NN controller is better than that of MOSMPS with conventional controller.

Inference: When the converter topologies for MOSMPS are compared based on their performances tabulated in Tables 4,5 and 6, it can be concluded that forward converter based MOSMPS with neural network controller performs better compared to other converter topologies in the following aspects: i)The output voltages are well regulated with lower values of output voltage ripple for all the output voltages under varying load conditions. ii) The supply current drawn is sinusoidal and in phase with the supply voltage with PF value nearly unity. When the supply voltage is 220V, the values of DF, DPF and PF are 0.996, 1.00 and 0.996 respectively. NN based forward converter has higher values of DF, DPF and PF when compared to other converter topologies under varying source and load conditions. iii) THD of the source current is lesser when compared to other converter topologies under varying source and load conditions. The THD of the source currents satisfy the limit set by the IEEE 519 and IEC 61000-3-2 standards even under varying source and load conditions. iv) The % overshoot and undershoot of output voltage at terminal 1(V_{o1}) are lesser for forward converter based MOSMPS when compared to other converter topologies. v) The settling time of forward converter based MOSMPS is lesser when compared to other converter topologies like cuk and flyback. The superior performance of the forward converter based MOSMPS with neural network controller can also be inferred from Fig. 17, 18 and 19. Fig. 17 shows the comparison of % THD of I_{in} for various converter topologies and supply voltage conditions with 100% and 50% loads at terminal 2. The %THD of I_{in} is lesser in all the converter topologies with NN controller when compared to conventional controller. Fig. 18 shows the comparison of input PF for various converter topologies at $V_{in}=220$ V with 100% and 50% load at terminal 2 and Fig. 19 shows comparison of settling time, % overshoot and % undershoot of V_{o1} at $V_{in}=220$ V. In terms of PF, settling time, % overshoot and %undershoot the performance of MOSMPS with NN controller is superior when compared to conventional controller.

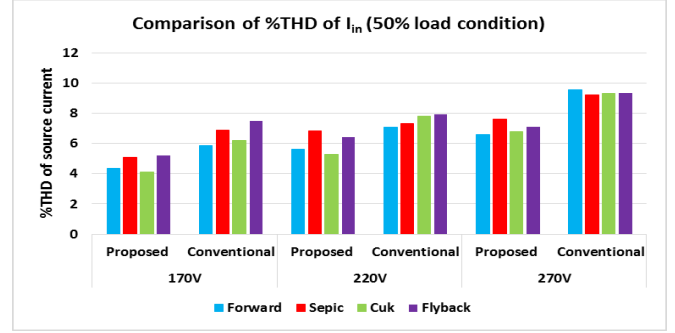
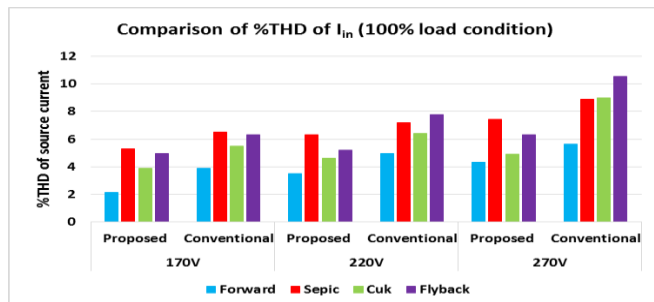


Fig. 17 Comparison of %THD of source current I_{in} . (a) 100% load condition (b) 50% load condition

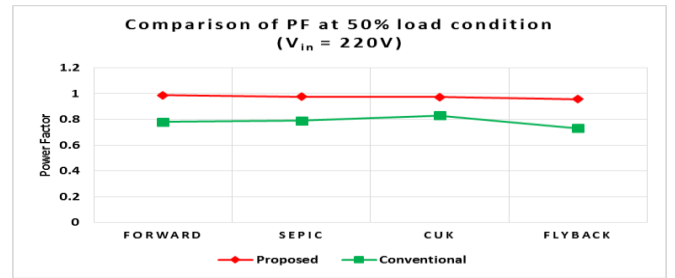
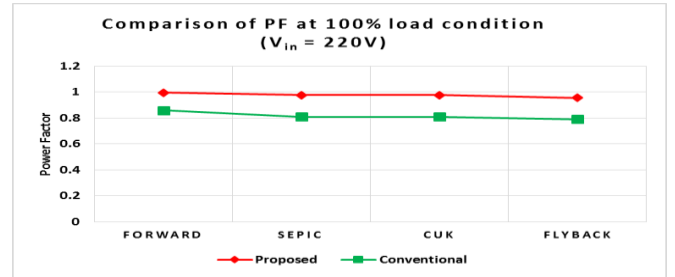
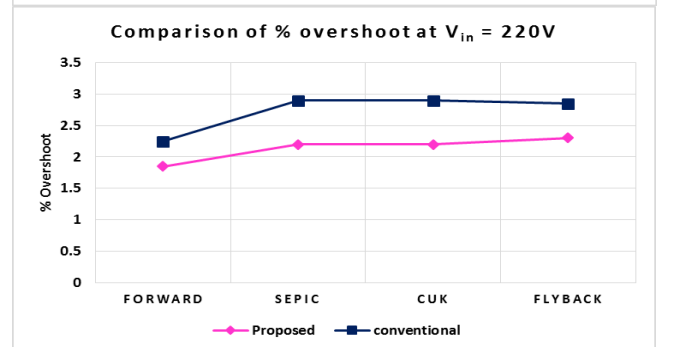
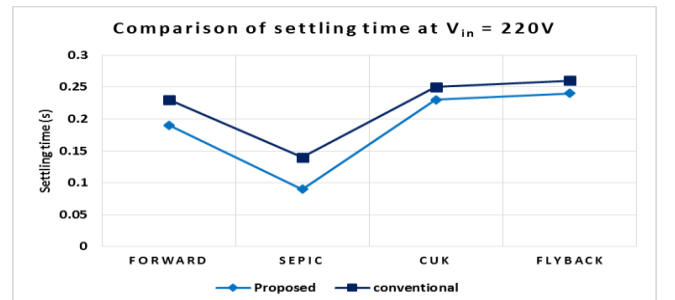


Fig. 18 Comparison of PF at $V_{in}=220$ V (a) 100% load condition (b) 50% load condition.



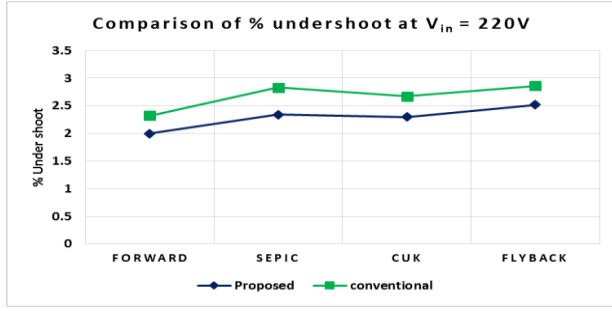


Fig. 19 Comparison of transient response of V_{o1} at $V_{in} = 220$ V. (a) settling time (s) (b) % overshoot (c) %undershoot

6. EXPERIMENTAL RESULTS AND DISCUSSIONS

Based on the simulation results, it is inferred that forward converter proves to be superior to other converter topologies of MOSMPS. Thus for hardware set up forward converter configuration is chosen. The design and simulated performance of the proposed NN controlled forward converter based MOSMPS are validated with the help of developed hardware. The results obtained from the developed hardware are compared with the simulation results to verify its performance in terms of power quality improvement and output voltage regulation. The proposed control strategy is implemented using FPGA processor (Spartan-6). A 50 kHz switching frequency is adopted to reduce the size of the components and to have effective control of the switch. The isolation between the control circuit and power circuit is provided by means of IC TLP250. Output voltages are sensed using HCPL 7840. Fig. 20 shows the photograph of the developed hardware. The test results are recorded with the help of power analyser Yokogawa WT 1800 and Digital Storage Oscilloscope (DSO).

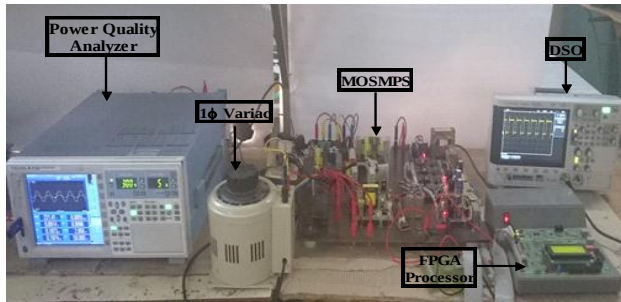


Fig. 20 Experimental set up.

6.1 Performance at rated load and supply voltage condition.

The performance of the proposed NN controlled forward converter based MOSMPS at full load condition with a supply voltage of $V_{in} = 220V$ is depicted in Fig. 21. Fig. 21 a depicts the source voltage and current waveforms at $V_{in} = 220V$ with rated load which infers that the MOSMPS draws sinusoidal current from the AC mains. The supply current is maintained in phase with the supply voltage thereby maintaining the PF at 0.9998. From the results it is evident that THD of the supply current I_{in} is 2.944% which complies

with the limits set by the International PQ standards. Fig. 21 b & c represent output voltages +12V, +5V, -12V and -5V and their corresponding output currents respectively. The constant output voltage waveforms clearly exhibit the output voltage regulation.

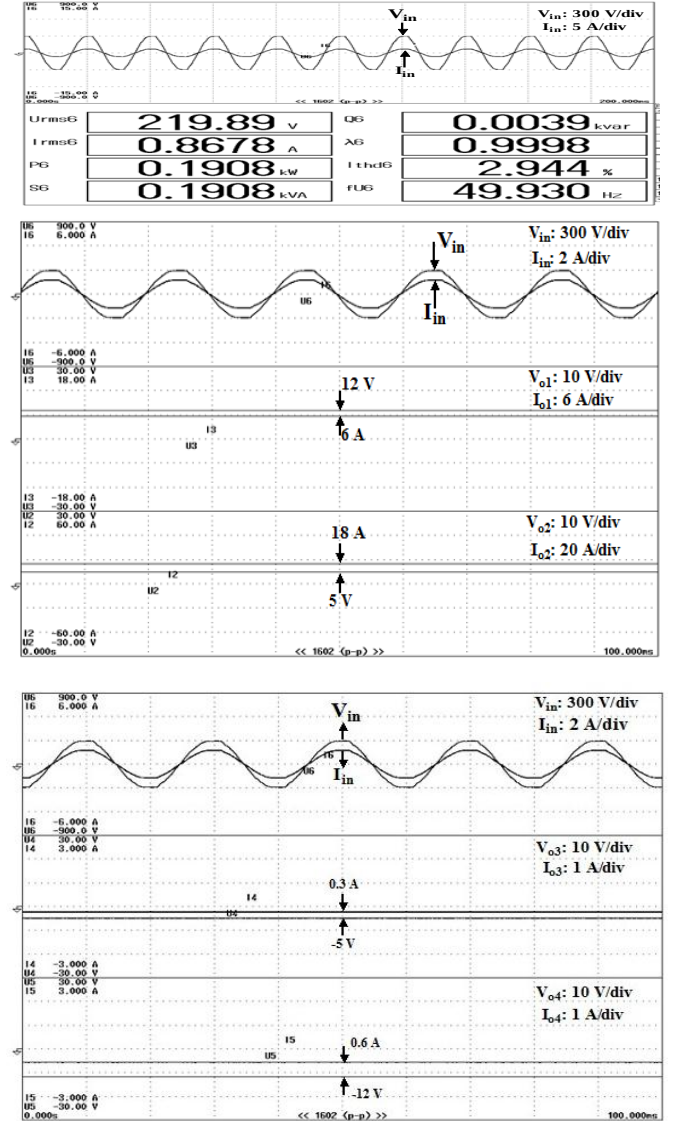


Fig. 21(a) Traces of V_{in} , I_{in} with input power, PF and % THD of I_{in} at full load, (b) Traces of V_{in} , I_{in} , V_{o1} , I_{o1} , V_{o2} and I_{o2} , (c) Traces of V_{in} , I_{in} , V_{o3} , I_{o3} , V_{o4} and I_{o4}

6.2 Performance under supply voltage variation with rated load.

When the proposed MOSMPS is supplied from the utility supply, it has to perform efficiently under supply voltage variations. To demonstrate its performance under varying source voltage conditions, the supply voltage is varied from 170V to 250V. When the supply voltage is reduced to 170V the PF and THD of the supply current are shown in Fig. 22 a. The THD of the supply current is maintained at 2.522%. When the supply voltage is increased to 250V the PF and THD of the supply current are represented in Fig. 22 b.

Even when the supply voltage is increased to 250V, the THD is maintained 2.924% which is less than the limits suggested by PQ standards. During over voltage and under voltage conditions of the supply, PF is maintained close to unity. The performance of the MOSMPS is appreciable under varying supply voltage conditions.

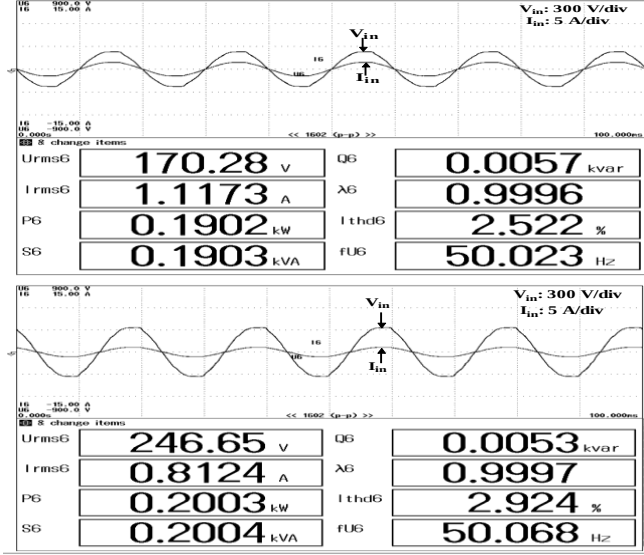


Fig. 22(a) Traces of V_{in} , I_{in} with input power, PF and % THD of I_{in} at $V_{in}=170V$, (b) Traces of V_{in} , I_{in} with input power, PF and % THD of I_{in} at $V_{in}=250V$

6.3 Performance under load variation with rated supply voltage.

To demonstrate the dynamic response of the proposed MOSMPS the load at V_{o2} is varied. The change in load is represented in the Fig.23a with output current decreasing from 16 A to 8 A. There is a corresponding reduction in the supply current and the supply current is maintained sinusoidal even after load reduction as shown in Fig. 23 b. The PF and THD are maintained at 0.99 and 2.767% as shown in Fig. 23e for light load condition. Fig. 23c shows the increase in load at terminal V_{o2} with an increase in load current from 8 A to 16 A. The traces of Fig. 23 d ensures that load current remains sinusoidal and in phase with the supply voltage thereby ensuring unity PF.

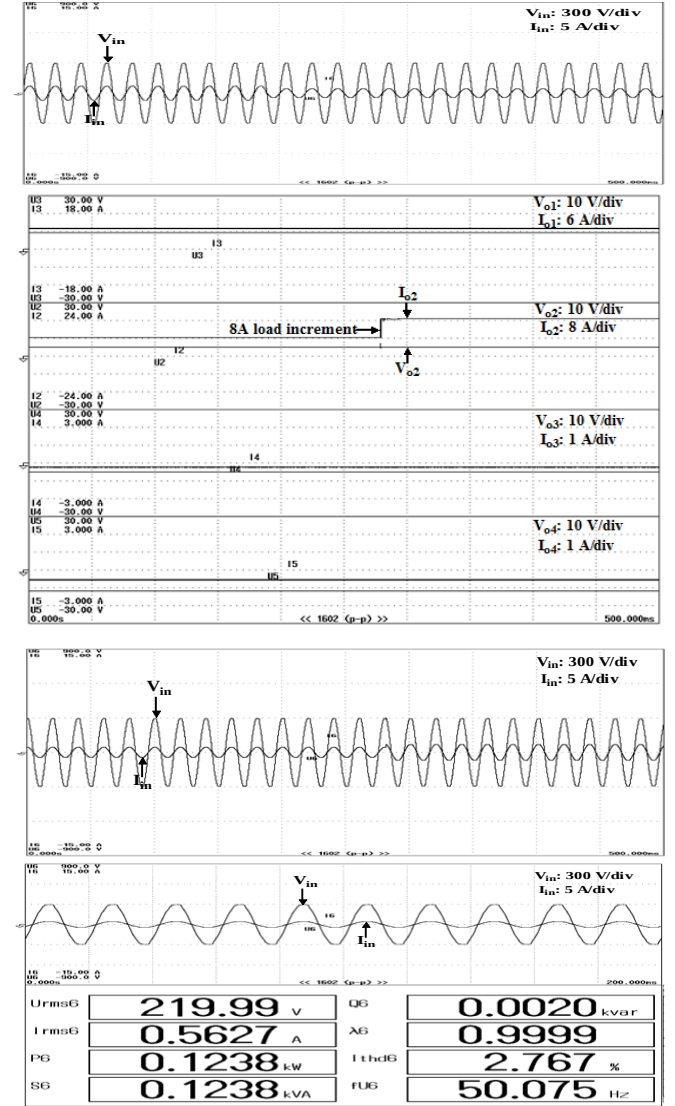
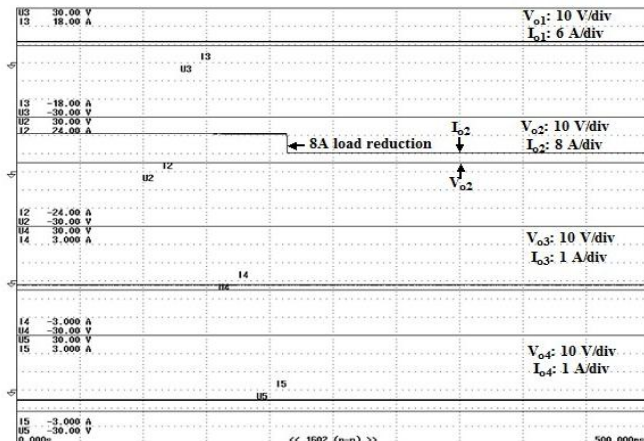


Fig. 23(a) Load reduction in +5V (b) Traces of V_{in} & I_{in} (load reduction), (c) Load increment in +5V, (d) Traces of V_{in} & I_{in} (load increment), (e) Traces of V_{in} , I_{in} with input power, PF and % THD of I_{in} at light load condition.

Table 7 clearly highlights the superior performance of the experimental setup of the neural network based forward converter MOSMPS when compared to the conventional controller based forward converter MOSMPS.

Table 7. Performance analysis of the experimental setup.

Supply Voltage (V)	PF		% THD of I_{in}	
	1*	2*	1*	2*
170	0.9996	0.8682	2.522	7.73
220	0.9998	0.7981	2.944	8.085
250	0.9997	0.8954	2.924	7.22

1*-NN Controller, 2*-Conventional Controller

The performance of the developed hardware validates the simulation results and its efficacy is proved in terms of input PQ improvement and output voltage regulation under varying source and load conditions.

7.CONCLUSIONS

Design, modeling, simulation and performance analysis of multi output SMPS with converter topologies like forward, sepic, cuk and flyback have been made to facilitate selection of suitable topology for the specific application. The performance of these topologies have been analysed in terms of input power quality, output voltage regulation and transient response under variation in source and load conditions. From the simulation traces and tabulated parameters, neural network controlled forward converter based MOSMPS prove to be the optimal choice in terms of THD of supply current, distortion factor, displacement factor, power factor, output voltage ripple, overshoot and undershoot. The experimental results from the prototype model and the simulation results verify the efficacy of the neural network controlled forward converter based multi output SMPS.

REFERENCES

- Buso, S., Spiazzi, G., and Tagliavia, D. (2000). Simplified control technique for high power factor flyback Cuk and Sepic rectifiers operating in CCM, *IEEE Trans. Ind. Appl.*, Vol. 36(5), pp. 1413-1418.
- Carlos Alberto Gallo, Fernando Lessa Tofoli, and Joao Antonio Correa Pinto. (2010). Two-stage isolated switch-mode power supply with high efficiency and high input power factor, *IEEE Trans. Ind. Electron.*, Vol. 57(11), pp. 3754–3766.
- Chow, M.H.L., Siu, K.W., Tse, C.K., and Lee, Y.S. (1998). A novel method for elimination of line-current harmonics in single-stage PFC switching regulators, *IEEE Trans. Power Electron.*, Vol. 13(1), pp. 75-83.
- Jingquan Chen, Maksimovic, D., and Erickson, R.W. (2006). Analysis and design of a low stress buck-boost converter in universal-input PFC applications, *IEEE Trans. Power Electron.*, Vol. 21(2), pp. 320–329.
- Jayachandran, J., and Murali Sachithanandam, R. (2015). Neural network based control strategy for hybrid DSTATCOM in three phase four wire distribution system under non-ideal voltage source conditions and varying load conditions, *International Review of Electrical Engineering*, Vol. 10(3), pp. 421-433.
- Jayachandran, J., and Murali Sachithanandam, R. (2015). Neural network based control algorithm for DSTATCOM under non ideal source voltage and varying load conditions, *CJECE*, Vol. 38(4), pp.307-317.
- Jayachandran, J., and Murali Sachithanandam, R. (2016). ANN based controller for three phase four leg shunt active filter for power quality improvement, *Ain Shams Engineering Journal*, Vol. 7, pp. 275-292.
- Moore, P.J., and Portugues, I.E. (2003). The influence of personal computer processing modes on line current harmonics, *IEEE Trans. Power Delivery*, Vol. 18(4), pp. 1363–1368.
- Sabha Raj Arya, Bhim Singh, Ambrish Chandra and Kamal Al-Haddad. (2014). Learning –based anit-hebbian algorithm for control of distribution static compensator, *IEEE Trans Ind. Electron.*, Vol. 61(11), pp. 6004–6012.
- Shika Singh, Bhim Singh, Bhuvaneswari, G., Vashist Bist , Ambrish Chandra, and Kamal Al-Haddad. (2015). Improved power quality bridgeless converter based multiple output SMPS, *IEEE Trans. Ind. Appl.*, Vol. 51(1), pp. 721–732.
- Singh, B., Singh, B.N., Chandra, A., Al-Haddad, A., Pandey, A., and Kothari, D.P. (2003). A review of single phase improved power quality AC-DC converters, *IEEE Trans. Ind. Electron.*, Vol. 50(5), pp. 962–981.
- Singh, B., Singh, S., Chandra A., and Al-Haddad, K. (2011). Comprehensive study of single phase AC-DC power factor corrected converters with high frequency isolation, *IEEE Trans. Ind. Informatics*, Vol. 7(4), pp. 540–556.
- Woo-Young Choi and Joo-Seung Yoo. (2011). A bridgeless single stage half bridge ac/dc converter, *IEEE Trans. Power Electron.*, Vol. 26(12), pp. 3884–3895.
- Zhao, Q., Lee, F.C., and Tsai, F. (2002). Voltage and current stress reduction in single stage power factor correction AC-DC converters with bulk capacitor voltage feedback, *IEEE Trans. Power Electron.*, Vol. 17(4), pp. 477-484.